Superprism phenomena in polymeric woodpile structures

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An analysis of the optical properties of photonic woodpile structures is presented. We demonstrate large superprism phenomena inside polymeric woodpile structures having a refractive index of less than \( n = 1.6 \). Due to the low contrast in refractive indices the structures investigated do not possess a complete photonic band gap. Nevertheless, their photonic band structures show strong anisotropy at frequencies slightly above the band gap in the (\( \Gamma-X \)) direction, leading to an extreme sensitivity to the angle and the frequency of the incident light in the propagation direction inside the crystal. Furthermore, if the woodpile structure is arranged in a prism-like shape, the transmitted beam outside the crystal shows a strong sensitivity to the frequency and angle of the incident light.

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I. INTRODUCTION

Recently the fabrication of woodpile structures having a photonic band gap in the near-infrared wavelength region by means of two-photon polymerization has been reported by several groups.\textsuperscript{1-7} Since the applied polymers have a refractive index of only \( n = 1.47 \) Ormocer’s\textsuperscript{8} to \( n = 1.56 \) Ormocer’s\textsuperscript{8} and SU8\textsuperscript{5}, the structures demonstrated only possess photonic band gaps (PBG’s) in certain directions. This technique cannot be utilized for the fabrication of complete PBG materials. Nevertheless, our simulations show that even in the absence of a complete PBG, the woodpile structure possesses extremely strong superprism properties. There have been several studies on the propagation properties of photonic crystals. Most of these investigations were carried out for two-dimensional lattices\textsuperscript{9-11} and only very few publications can be found on three-dimensional (3D) crystals.\textsuperscript{12} To calculate the propagation properties inside the woodpile structures we chose a method that was first suggested by Kosaka \textit{et al.},\textsuperscript{13,14} utilizing the complete photonic band structure. The calculations of the band structures shown within this work have been performed by means of the freely available software package MPB (Ref. 15) utilizing the plane wave method.

II. THE WOODPILE STRUCTURE

A sketch of a woodpile structure is shown in Fig. 1. The crystal consists of layers of one-dimensional rods with a stacking sequence that repeats itself every four layers. The distance between four adjacent layers is denoted by \( c \). Within each layer, the axes of the rods are parallel to each other with a distance \( d \) between them. The adjacent layers are rotated by 90\textdegree. Between every other layer, the rods are shifted relative to each other by \( d/2 \). Generally, the resulting structure has a face-centered-tetragonal (fct) lattice symmetry. For the special case of \( c/d = \sqrt{2} \), the lattice can be derived from a face-centered-cubic (fcc) unit cell with the basis of two rods.\textsuperscript{16} The following calculations all were accomplished for crystals having fcc symmetry.

III. COMPLETE BAND STRUCTURES OF POLYMERIC WOODPILE STRUCTURES

Figure 2 shows the calculated band structure for a woodpile structure having a contrast in the refractive index of \( n = 1.47 \). The rods of the respective structure have an elliptical cross section. The width and the height of the rods are \( w = 0.3d \) and \( h = 0.7d \), respectively, where \( d \) is the in-layer rod spacing (see Fig. 1, top). The band structure is shown for a path along high symmetry points within the irreducible Brill-
The band structure was calculated for a resolution of the following calculations vectors directing from the \( \Gamma \) point to the respective directions. The band structure was calculated for \( k \) vectors within the triangles. For each direction, the magnitude of the \( k \) vectors was varied in steps of \( \bar{d} \) with a gap to mid-gap ratio of 3.6%. To determine the propagation properties inside the woodpile structure, the complete photonic band structure has to be determined by the high symmetry points \( X-U-W, L-U-W, \) and \( L-K-W \), and each of these triangles was divided into 861 \( k \) points (the number of \( k \) points determines the resolution of the following calculations), representing the respective directions. The band structure was calculated for \( k \) vectors directing from the \( \Gamma \) point to the respective \( k \) value within the triangles. For each direction, the magnitude of the \( k \) vectors was varied in steps of \( |k_{max}|/30 \). In more simple fcc crystals like the artificial opal, where the primitive lattice cell only contains one single sphere at the origin, the surface of the entire Brillouin zone can be described by one set of such three triangles due to symmetry properties. Since the primitive cell of a woodpile structure is based on two perpendicular rods, not all of those symmetry conditions are valid anymore, and to cover the entire surface of the Brillouin zone, the calculations have to be carried out for three sets of triangles (i.e., \( XUW, LUW, LKW, X'U'W', LU'W', LKW' \), and \( X'U'W'', LU'W'', LKW'' \); see Fig. 3).

This allows us to determine \( \omega(k) \) for all values of \( k \) within the Brillouin zone. To understand the refraction properties of the woodpile structure it is useful to determine \( k(\omega) \), which is the inverse problem. To solve this, \( \omega(k) \) was inverted numerically, allowing us to calculate the iso energy surfaces (IESs) \( k(\omega) \) for fixed frequencies \( \omega \).

The IESs for a woodpile structure having a contrast in the refractive index of \( \Delta n = 1.47 \) are shown in Fig. 4 for normalized frequencies of \( \omega = 0.40 \) (second band) and \( \omega = 0.68 \) (fourth band). As one would expect, the woodpile structure behaves like a homogeneous medium with an effective refractive index for frequencies far below the band gap, leading to a spherical-shaped IES (the left image in Fig. 4). The radius of the sphere, which determines the magnitude of the wave vector, is \( |k| = 0.676 \), which corresponds to a group velocity of \( |v_{\text{group}}| = c/n_{\text{eff}} \). For frequencies slightly above the band gap, the strong anisotropy of the dispersion relation, which leads to a star-like shape of the IES, becomes obvious (the right image in Fig. 4). Since the direction of the group velocity (as well as the direction of energy flow) of the propagating light are determined by the gradient of \( \omega \) with respect to \( k (\nabla k \omega) \), the surface normals of the IES determine the propagation direction inside the photonic crystal \( 14 \) and generally point to another direction as the respective \( k \) vector leading to the superprism phenomenon. These internal propagation properties will be investigated in a more detailed way in the following section.

IV. PROPAGATION INSIDE THE WOODPILE STRUCTURE

The following calculations were performed for light incident to the (001) plane of the woodpile structure (see Fig. 1, lower image) at an azimuth angle of \( \theta = 45^\circ \). Due to the conservation of the parallel component of the \( k \) vector at the transition from one medium to another, the light inside the crystal will be confined to the \( (\bar{1}10) \) plane, as indicated in the sketch, i.e., the parallel component \( k_{\parallel} \) points in the direction of the rods and the normal component \( k_{\perp} \) points in the stacking direction. In the following the propagation inside the crystal will be investigated as a function of the elevation angle \( \phi \) and the normalized frequency \( \omega \).

Figure 5 shows the internal propagation angle \( \phi_{\text{prop}} \) as a function of the normalized frequency for different angles of incidence. The shown simulations were performed with a contrast in a refractive index of \( \Delta n = 1.47 \). To obtain \( \phi_{\text{prop}} \) the wave vectors \( k \) for the propagating light were calculated numerically utilizing the complete photonic band structure, taking the conservation of the parallel component into account. Subsequently, the direction of propagation was obtained by determining the vector normal to the IES at the respective \( k \) point. For frequencies slightly above the band gap, the woodpile structure shows negative refraction (\( \phi_{\text{prop}} \approx -11^\circ \)), a phenomenon that has recently been discussed by several groups. \( 18-20 \) With increasing frequency, the propagating angles show a shift to positive values of \( \phi_{\text{prop}} \approx 79^\circ \). The...
frequency of high sensitivity varies with the angle of the incident light, as shown for $\phi_{\text{in}} = 21^\circ$ to $25^\circ$. These values are of the same order as reported for inverted artificial opal structures.\(^{21}\)

It has been demonstrated that woodpile structures for the near infrared can be fabricated by means of two-photon polymerization of hybrid polymers (ORMOCERs), which have a refractive index that can be tuned by means of chemical design between $n=1.47$ and $n=1.56$. Figure 6 shows how the frequency of high sensitivity changes with a variation of the refractive index within those values. Although the gap to mid-gap ratio of the PBG decreases from 4.7\% to 3.6\% when changing the refractive index from $n=1.56$ to $n=1.47$, the change in magnitude of the angular shift is negligible.

All of the data shown were calculated in terms of normalized frequencies $\omega = d/\lambda$. It has been demonstrated by several groups that woodpile structures can be fabricated by means of two-photon polymerization with in-layer rod distances of 1 \(\mu\)m and below,\(^{5-7}\) which would lead to strong superprism effects at wavelengths of about 1.5 \(\mu\)m. A woodpile structure having an in-layer rod distance of $d=0.8$ \(\mu\)m, for example, would exhibit a shift in the propagation angle from $\phi_{\text{prop}} \approx -11^\circ$ to $\phi_{\text{prop}} \approx 78^\circ$ within a range of wavelengths reaching from $\lambda = 1.55$ \(\mu\)m to $\lambda = 1.50$ \(\mu\)m at an incident angle of $\phi_{\text{in}} = 22^\circ$. This corresponds to a sensitivity of $17.8^\circ/\text{nm}$.

V. PROPAGATION OUTSIDE THE WOODPILE STRUCTURE

In the previous section, the propagation of light inside the woodpile structure has been discussed and strong sensi-
activity of the propagating angles on the frequency and the angle of incidence has been observed. However, from the experimental side of view, the light that is transmitted by the photonic crystal structure is much more easily accessible than the light inside the crystal. The propagation direction of the transmitted light can be derived in the same manner as the light inside the crystal, with the only difference that two tilted interfaces have to be considered now.

Figure 7 shows schematically how the direction of the transmitted light can be determined for a woodpile prism with an opening angle $\alpha$. The plot shows an isoenergy contour (IEC) for a (110) plane in the woodpile structure (\(\theta =45^\circ\)). This plane is defined by the $z$ axis and the bisector of the $x$-$y$ plane ($\sqrt{k_x^2+k_y^2}$). The $k$ vector for the light propagating inside the crystal $k_{\text{prop}}$ is determined by the intersection of the vertical (dash-dotted) line and the IEC, leading to conservation of $k$. To obtain the $k$ vector and hence the direction of propagation outside the crystal one has to take the conservation of $k$ into account, this time with respect to the second interface that is tilted by an angle of $\alpha$, leading to $k_{\text{out}}$. The output angle $\phi_{\text{out}}$ will be treated as the angle between $k_{\text{out}}$ and the normal to the input surface (rather than the output surface).

Due to this construction scheme, it is obvious that the direction of propagation outside the crystal is independent of the propagation direction inside the crystal, since only $k$ vec-

FIG. 7. Isoenergy contour [intersection of the IES with the (110) plane] for a polymeric woodpile structure at a normalized frequency of $\omega=0.64$ and a sketch of a woodpile prism.
Nevertheless, a strong sensitivity of the propagating angle of the incident light from woodpile structures of arbitrary prism shapes and also to direct laser writing method, it is straightforward to fabricate PBG structures. We have investigated the propagation properties of these structures theoretically. The angles of the light propagating inside woodpile structures is very sensitive to the frequency and the angle of incidence. A sensitivity of up to 17.8°/nm at a wavelength of 1.3 μm for a photonic crystal with an in-layer rod spacing of 1 μm was shown. If the woodpile structure is designed in a prism-like shape, superprism effects can also be observed outside the woodpile structure with a sensitivity of 0.16°/nm. Since two-photon polymerization is a truly 3D direct laser writing method, it is straightforward to fabricate woodpile structures of arbitrary prism shapes and also to integrate them into 3D waveguide structures. This opens a wide field of applications for very compact devices such as dense wavelength division multiplexers.

VI. CONCLUSION

We have demonstrated strong superprism effects inside photonic woodpile structures at frequencies slightly above the band gap. The calculations were performed for structures that have already been realized by several groups, with the main intention of fabricating PBG structures. We have investigated the propagation properties of these structures theoretically. The angles of the light propagating inside woodpile structures is very sensitive to the frequency and the angle of incidence. A sensitivity of up to 17.8°/nm at a wavelength of λ ≈ 1.3 μm for a photonic crystal with an in-layer rod spacing of 1 μm was shown. If the woodpile structure is designed in a prism-like shape, superprism effects can also be observed outside the woodpile structure with a sensitivity of 0.16°/nm. Since two-photon polymerization is a truly 3D direct laser writing method, it is straightforward to fabricate woodpile structures of arbitrary prism shapes and also to integrate them into 3D waveguide structures. This opens a wide field of applications for very compact devices such as dense wavelength division multiplexers.

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